

**Process for Laser Welding Poly(ethylene terephthalate)**

**Cross Reference to Related Applications**

This application claims the benefit of U.S. Provisional Application No.  
5 60/406,885 filed August 29, 2002.

**Field of the Invention**

This invention relates to an improved process for laser welding parts  
comprising poly(ethylene terephthalate) and one or more nucleating agents that have  
10 low levels of moisture absorption.

**Background of the Invention**

It is often desired to produce molded plastic parts that can be mechanically  
assembled into more complex parts. Traditionally, plastic parts have been  
15 assembled by gluing or bolting them together or using snap-fit connections. These  
methods suffer from the drawback that they add complex additional steps to the  
assembly process. Snap-fit connections are often not gas- and liquid-tight and  
require complex designs. Newer techniques are vibration and ultrasonic welding, but  
these can also require complex part designs and welding apparatuses. Additionally,  
20 the friction from the process can generate dust that can contaminate the inside of the  
parts. This is a particular problem when sensitive electrical or electronic components  
are involved.

A more recently-developed technique is laser welding. In this method, two  
polymeric objects to be joined have different levels of light transmission at the  
25 wavelength of the laser that is used. One object is at least partially transparent to the  
wavelength of the laser light (and referred to as the "relatively transparent" object),  
while the second part absorbs a significant portion of the incident radiation (and is  
referred to as the "relatively opaque" object). Each of the objects presents a faying  
surface and the relatively transparent object presents an impinging surface, opposite  
30 the faying surface thereof. The faying surfaces are brought into contact, thus forming  
a juncture. A laser beam is directed at the impinging surface of the relatively  
transparent object such that it passes through the first object and irradiates the faying  
surface of the second object, causing the first and second objects to be welded at the  
juncture of the faying surfaces. See generally U.S. Patent 5,893,959, which is  
35 hereby incorporated by reference herein. This process can be very clean, simple,

and fast and provides very strong, easily reproducible welds and significant design flexibility.

The degree to which a material will transmit incident laser radiation is a function of not only the chemical compositions of the components of the material, but the arrangement of the components within the material. For example, if the material is a polymer matrix containing dispersed additives that have a large enough average particle size, these particles can scatter incident radiation, which will lower the light transmission rates, even if the components of the material don't absorb the radiation.

In order to generate a strong weld, it is preferable that the two objects be made from thermoplastic materials. Due to their excellent physical properties, semicrystalline polyesters are often used to produce parts for assembly by the various methods mentioned above. It would also be desirable to use polyesters in laser-welding applications; however to do so, it is necessary that a polyester composition be available that has a high degree of transmittance of laser light at a wavelength suitable for laser welding.

Poly(ethylene terephthalate) homopolymer and its semicrystalline copolymers (referred to collectively as "PET") are slow to crystallize, and hence difficult to mold. They require long molding cycle times, which confers significant economic disadvantages. As a result, a nucleating agent is often added to the polymer to speed up crystallization and shorten cycle times.

A further advantage of semicrystalline polyesters is that they have low levels of moisture absorption, which means that parts made from PET have few problems with surface blistering when heated or used over time. However, when certain additives are blended with polyesters, they can absorb significant amounts of moisture, which can lead to surface blistering and degradation over time. This is a particular problem in laser welding applications, as this blistering and degradation will damage the appearance and or mechanical integrity of the weld.

Thus, it would be highly desirable to obtain a PET composition that has good moldability, good weldability, and which is highly resistant to absorbing moisture.

### **Summary of the Invention**

The present inventor has discovered that by limiting the type of nucleating agents used in combination with PET, for instance certain nucleating agents that absorb no more than 7% of their weight in water, they are able to obtain a PET composition that has good moldability and good laser weldability.

In accordance with the present invention, there is disclosed an improvement in a welding process for welding a first polymeric object to a second polymeric object

utilizing laser radiation, wherein said first polymeric object is relatively transparent to said laser radiation and said second object is relatively opaque to said laser radiation, said first and second objects each presenting a faying surface, said first object presenting an impinging surface, opposite said faying surface thereof; said process including the steps of bringing the faying surfaces of said first and second objects into physical contact so as to form a juncture therebetween and irradiating said first and second objects with said laser radiation such that said laser radiation impinges the impinging surface, passes through said first object and irradiates said faying surface of said second object, causing said first and second objects to be welded at the juncture of the faying surfaces, the improvement comprising:

said first polymeric object being formed from a polymeric component comprising: (i) poly(ethylene terephthalate); and

(ii) one or more nucleating agents;

said one or more nucleating agents each being characterized in the fact that they absorb no more than 7% of their weight in water;

said one or more nucleating agents being present in said polymeric component in an amount sufficient such that said polymeric component has a crystallization half time of less than 20 minutes at a temperature of 105 °C when measured by differential scanning calorimetry; and

said first polymeric object exhibits, through a thickness between said faying surface of said first object and said impinging surface, a diffuse transmittance of at least 15% of said laser radiation.

Laser-welded articles made from the method of the invention are also disclosed herein.

### **Brief Description of the Drawings**

Figs. 1, 2 and 3 are a side elevation, top plan view and a perspective view, respectively, of a test piece 11 for measuring weld strength as reported herein.

Fig. 4 is a perspective view of test pieces 11', a relatively transparent object and 11", a relatively opaque object, having their respective faying surfaces in contact and placed in position for a laser welding.

### **Detailed Description of the Invention**

It has been discovered that a PET composition for use in forming laser weldable parts in accordance with the invention can be obtained when the PET is

melt-blended with a suitable nucleating agent, i.e. one that is easily dispersed into the PET and picks up little moisture from the atmosphere.

By "poly(ethylene terephthalate)" or "PET" herein is meant poly(ethylene terephthalate) homopolymer, copolymers of poly(ethylene terephthalate) derived from one or more additional monomers, a blend of the homopolymer with one or more such copolymers or a blend of two or more such copolymers. The copolymer may contain up to about 15 mole percent of one or more additional monomers such that the copolymer is semicrystalline. In order to be considered semicrystalline, the copolymer must have a heat of fusion of at least 5 J/g. Herein heats of fusion are determined by ASTM D3418-82, at a heating rate of 20 °C/min. The peak of the melting endotherm is taken as the melting point. The heat of fusion is taken as the area under the melting endotherm. All of these are measured on the second heat, meaning that the sample is heated at 20 °C/min until the melting point and/or glass transition point, whichever is higher, is exceeded, and then the sample is cooled at 20 °C/min to 30 °C. The heating cycle is begins again and measurements are then taken on a second heat, also done at 20 °C/min. Suitable comonomers include, but are not limited to, isophthalic acid and its functional equivalents, naphthalene dicarboxylic acid and its functional equivalents, 1,3-propane diol, 1,4-butane diol, cyclohexanedimethanol, di(ethylene glycol), and ethoxylated bisphenol A. Preferred is isophthalic acid.

A wide range of materials are suitable for use as nucleating agents for PET as taught in the following references and references contained therein: R. Legras, C. Bailly, M. Daumerie, J. M. Dekoninck, J. P. Mercier, V. Zichy, E. Nield *Polymer* **1984**, 25, 835; J. W. Glimer; R. P. Neu; Y. J. Liu; A. K.-Y. Jen *Polymer Engineering & Science* **1995**, 35, 1407; D. Garcia *J. Poly. Sci. Poly. Phys. Ed.* **1984**, 22, 2063; US Patent Re. 32,334. Effective nucleating agents for PET are generally materials that are capable of transferring sodium ions to the PET.

The nucleating agent used in the present invention has a low level of moisture absorption as determined by a method described below. The nucleating agent will gain less than 7%, or preferably less than 5%, or more preferably less than 4%, or still more preferably less than 3%, or even more preferably less than 2%, or yet more preferably less than 1% of its weight under such conditions.

It is also preferred that the nucleating agent can be conveniently well-dispersed into the polymer. If it forms domains that are too large, they may scatter so much incident light that the resulting material will not be transparent for purposes of laser welding. The transparency of a material is determined by measuring the diffuse transmittance of a given thickness of a sample of the blend. If the sample at

the given thickness has a diffuse transmittance of at least 15% at the frequency of the laser, it is usually suitable for laser welding at that frequency and thickness.

Suitable nucleating agents are compounds with number average molecular weights of less than about 5000, preferably less than about 2000, that are preferably molten under melt-mixing conditions and thus disperse thoroughly, and that absorb low levels of moisture, such as sodium montanate, sodium stearate, and other sodium neutralized aliphatic carboxylic acids with 12-40 carbon atoms. By "sodium neutralized aliphatic carboxylic acid" is meant a sodium salt of an aliphatic carboxylic acid.

Trisodium phosphate can be well-dispersed into small particles that do not scatter enough light to interfere with laser welding, but it absorbs a significant amount of moisture, which leads to blistering and/or the degradation of a laser weld, which renders it unsuitable for use in this invention.

Most polymeric nucleating agents are not useful because they tend to form large domains that scatter light. For example, common general-purpose nucleating agents for PET are sodium neutralized ethylene/methacrylic acid copolymers as taught in US Patent Re. 32,334. However, sodium neutralized ethylene/methacrylic acid copolymers are not compatible with PET and form large domains that scatter enough light to render them unsuitable as components for a transparent laser welding part when they are used in high enough loadings to be effective as nucleating agents.

An acceptable polymeric nucleating agent is sodium PET, where "sodium PET" refers to PET in which the protons of some of the acid end groups have been replaced with sodium ions. Sodium is typically present in the sodium PET about 0.10 to about 0.40 weight percent based on the weight of the PET.

The nucleating agent of this invention is preferably present in an effective amount to provide good moldability. To determine whether any particular amount is an effective amount, the crystallization half times of blends of the compositions of this invention are determined using a method described below. Samples that have crystallization half times of less than 20 minutes at 105 °C in this test are considered to be effectively nucleated.

The composition used in the present invention may also include up to 50 weight percent based on the total amount of polymer of one or more additional polymers such as polycarbonate, polyarylate, poly(ethylene naphthalate), poly(butylene terephthalate), and poly(butylene terephthalate) copolymers, as long as the presence of these additional polymers does not reduce the optical transmittance of the material to a point at which laser welding is unfeasible.

The composition used in the present invention may also contain up to 3 weight percent of a compound or resin containing two or more epoxy groups, such as a condensation product of epichlorohydrin and bisphenol A.

Further, the composition used in the present invention may contain additional  
5 additives such as inorganic fillers and reinforcing agents such as glass fibers, hollow spheres, bead, flake, or milled glass; flame retardants; pigments; dyes; other colorants; plasticizers; impact modifiers; lubricants; mold-release agents; heat stabilizers; antioxidants; viscosity modifiers; and UV stabilizers, as long as the presence of these additional polymers does not reduce the optical transmittance of  
10 the material to a point at which laser welding is unfeasible. Preferred additives are chopped glass fibers, which may be present in from about 5 to about 50 weight percent based on the total composition.

The compositions used in the present invention are in the form of a blend, wherein all of the non-polymeric ingredients are homogeneously dispersed in and  
15 bound by the polymer matrix, such that the blend forms a unified whole. The blend may be obtained by combining the component materials using any melt-mixing method. The component materials may be mixed to homogeneity using a melt-mixer such as a single or twin-screw extruder, blender, kneader, Banbury mixer, etc. to give a resin composition. Or, part of the materials may be mixed in a melt-mixer, and the  
20 rest of the materials may then be added and further melt-mixed until homogeneous.

Molding of the polyester compositions used in the present invention into parts for laser welding can be carried out according to methods known to those skilled in the art. Preferred are commonly used melt-molding methods such as injection molding, extrusion molding, blow molding, and injection blow molding.

25 The present invention also includes any laser welded article made from the process of the invention. Useful articles are housings, including those for electrical and electronic sensors, automotive fittings and headlamp housings, pumps, motors, valves, displays, connectors, couplings, and inkjet cartridges.

30

## **Examples**

### **General Procedures**

#### **Nucleating Agent Moisture Absorption Test**

35 A 5 g sample of the nucleating agent is dried in a vacuum oven at about 560 torr with a slow nitrogen bleed at 150 °C for 4 hours. The sample is then cooled in a desiccator, weighed, and held at 50% relative humidity (RH) and 23 °C for 24 hours.

The sample is then reweighed and the weight percent of moisture uptake relative to the dried sample is determined.

#### Compounding and Molding

5           The resin mixtures were prepared by compounding on a 30mm Werner and Pfleiderer twin-screw extruder at rate of 50 pounds per hour and 300 RPM. The glass fibers were side-fed and, as will be understood by those skilled in the art, the screw design is typical of those used for making glass-reinforced polyesters. The barrel temperatures were set to 280 °C and melt temperatures were usually about  
10       320 °C. Exiting the extruder, the polymer was passed through a die to form strands that were frozen in a quench tank and subsequently chopped to make pellets.

          The compounded product was dried and then molded using laboratory size injection molding machines into typical ASTM testing bars as well as the bars required for the laser welding tests as explained below. Barrel temperatures were  
15       set to 280 °C and the mold temperature was 110 °C.

#### Mechanical Properties

          Tensile strengths (TS) and percent elongations at break were determined using ASTM method D-638.

20

#### Light Transmittance

          Light transmittance was determined using a Varian® Cary® 5 spectrophotometer. A 940 nm light source was directed at a 2 mm thick molded sample and the diffuse light transmittance was measured within a 150 mm diameter  
25       integrating sphere. Alternatively, diffuse light transmittance was determined using a Shimadzu® UV-3100 spectrophotometer using a 120 mm diameter integrating sphere. The results from these two instruments were consistent to within about 1%.

#### Laser Weld Strength

30           Referring now to the drawings and in particular Fig. 1 - 3, there is disclosed the geometry of the test pieces 11 used to measure weld strength as reported herein. The test pieces 11 are generally rectangular in shape, having dimensions of 70 mm X 18 mm X 3 mm and a 20 mm deep half lap at one end. The half lap defines a faying surface 13 and a shoulder 15.

35           Referring now to Fig. 4, there is illustrated a pair of test pieces, 11' and 11", that are, respectively, a relatively transparent polymeric object and a relatively opaque polymeric object. The faying surfaces 13' and 13" of pieces 11' and 11" have

been brought into contact so as to form a juncture 17 therebetween. Relatively transparent piece 11' defines an impinging surface 14' that is impinged by laser radiation 19 moving in the direction of arrow A. Laser radiation 19 passes through relatively transparent piece 11' and irradiates the faying surface 13" of relatively opaque piece 11", causing pieces 11' and 11" to be welded together at juncture 17, thus forming a test bar, shown generally at 21.

In accordance with the invention, relatively transparent compositions (as disclosed in Examples 2 - 9) were dried and molded into test pieces that were conditioned at 23 °C and 65% relative humidity for 24 hours. By way of comparison (as disclosed in Comparative Examples B - G) compositions outside the scope of the present invention were also molded into test pieces, 11. A relatively opaque composition, made from Rynite® 530 BK, a 30% glass reinforced PET containing carbon black manufactured by E.I. DuPont de Nemours, Inc. Wilmington, DE, was similarly dried and molded into test pieces 11". Test pieces 11' and 11" and test pieces 11 and 11" were then welded together as described above, with a clamped pressure of 0.3 MPa therebetween to form test bars 21. Laser radiation was scanned in a single pass across the width of test pieces 11' and 11 at 500 cm/min with a Rofin-Sinar Laser GmbH 940 nm diode laser operating at 50 W. The test bars were further conditioned for 24 hours at 23 °C and 65% relative humidity. The force required to separate test pieces 11' and 11" and 11 and 11" was determined using an Instron® tester clamped at the shoulder of the test bars, applying tensile force in the longitudinal direction of the test bars 21. In Tables 2, 3, and 5 a value of at least 10 MPa indicates a good laser weld.

#### Crystallization Half Time

The crystallization half times of melt-blends of the compositions of this invention are determined using a differential scanning calorimeter (DSC). A 6-8 mg sample cut from the middle section of a molded bar is heated at 50 °C/minute in a DSC to 290 °C and held for 3 minutes then quenched in liquid nitrogen. The sample is then transferred to the cell of a Perkin-Elmer® DSC-7 or other DSC that can be heated very quickly to a set temperature and maintain that temperature, without significant temperature overshoot. The initial temperature of the DSC is set to zero, and upon addition of the sample, the cell is heated to 105 °C at 200 °C/min and held at 105 °C. The exotherm corresponding to crystallization is measured by the DSC as a function of time. The time corresponding to the maximum of the exotherm is assigned to be the crystallization half time. Samples that have crystallization half times of less than 20 minutes at 105 °C in the test are considered to be effectively

nucleated. Results for Examples 2, 3, and 6 and Comparative Example B are shown in Table 4. Samples from Examples 2, 3, and 6 were run in duplicate.

5     **Moldability**

          In Table 2, the level of moldability was deemed to be good if a cycle time of no more than 45 seconds could be achieved while molding standard ASTM tensile bars using a laboratory-scale molding machine.

10    **Materials Used**

          The materials used in the tables describing the examples are identified as follows:

Crystar® 3934 is a 0.67 inherent viscosity PET homopolymer manufactured by E.I. DuPont de Neumours, Inc., Wilmington, DE.

15    Crystar® 3931 is a PET copolymer containing 3 mole percent isophthalic acid manufactured by E.I. DuPont de Neumours, Inc., Wilmington, DE.

PET with IPA is a 0.9 inherent viscosity PET copolymer containing 1.6 mole percent of isophthalic acid.

HiPERTUF® 92004 is a poly(ethylene naphthalate) manufactured by M&G Polymers USA, LLC., Houston, TX.

20    Crastin® 6150 is a poly(butylene terephthalate) copolymer manufactured by E.I. DuPont de Neumours, Inc., Wilmington, DE containing 7.5 mole percent of Dianol® 220, an ethoxylated bisphenol A manufactured by Akzo Nobel Chemicals, Inc., Chicago, IL.

PTS is pentaerythritol tetrastearate.

25    EPON® 1009F is an epichlorohydrin/bisphenol A condensation product manufactured by Resolution Performance Products, Houston, TX.

NAV 101 is sodium montanate manufactured by Clariant, Inc., Charlotte, NC.

Surlyn® 8920 is a sodium neutralized ethylene/methacrylic acid copolymer manufactured by E.I. DuPont de Neumours, Inc., Wilmington, DE.

30    Irganox® 1010 is an antioxidant manufactured by Ciba Specialty Chemicals, Inc., Tarrytown, NY.

PPG 3563 is glass fibers manufactured by PPG Industries, Inc. Pittsburgh, PA.

5

**Table 1**

	<b>Ex. 1</b>	<b>Comp. Ex. A</b>
Nucleating agent	NAV 101	Trisodium phosphate
Weight after drying (g)	4.993	4.875
Weight after 24 h at 50% RH and 23 °C (g)	5.016	6.338
Percent weight gain	0.45	30.0

**Tabl 2**

	<b>Ex. 2</b>	<b>Ex. 3</b>	<b>Ex. 4</b>	<b>Ex. 5</b>	<b>Ex. 6</b>	<b>Ex. 7</b>
Crystar® 3934	83.2					
Crystar® 3931		83.2			58.2	58.2
PET with IPA			83.2	83.2		
HiPERTUF® 92004					10	
Crastin® 6150						10
PTS	0.5	0.5	0.5	0.5	0.5	0.5
EPON® 1009F	0.6	0.6	0.6	0.6	0.6	0.6
NAV 101	0.5	0.5	0.5		0.5	0.5
Sodium stearate				0.5		
Irganox® 1010	0.2	0.2	0.2	0.2	0.2	0.2
PPG 3563	15	15	15	15	30	30
TS (MPa)	106	102	98	96	128	119
Elongation (%)	3.4	3.5	3.6	3.5	2.3	2.5
Transmittance (%)	46	47	45	44	29	30
Weld Strength (MPa)	15	16	14	16	22	23
Moldability	Good	Good	Good	Good	Good	Good

5 All ingredient quantities are given in weight percent based on the total composition.

**Table 3**

	<b>Comp. Ex. B</b>	<b>C mp. Ex. C</b>	<b>C mp. Ex. D</b>	<b>C mp. Ex. E</b>
Crystar® 3934	83.2	80.7		
Crystar® 3931			70.9	
PET with IPA				65.9
HiPERTUF® 92004			10	
PTS	0.5	0.5	0.5	0.5
EPON® 1009F	0.6	0.6	0.6	0.6
Surlyn® 8920	0.5	3	3	3
Irganox® 1010	0.2	0.2		
PPG 3563	15	15	15	30
TS (MPa)	101	99	97	129
Elongation (%)	3.6	3.5	3.6	2.6
Transmittance (%)	38	12	11	6
Weld Strength (MPa)	16	2	3	3
Moldability	Poor	Good	Good	Good

5

All ingredient quantities are given in weight percent based on the total composition.

**Table 4**

10

	<b>Crystallization half time (min)</b>	
	<b>Sample 1</b>	<b>Sample 2</b>
Example 2	2.35	2.27
Example 3	2.43	2.42
Example 6	9.58	11.15
Comparative Example B	26.78	

**Table 5**

	<b>Ex. 8</b>	<b>Comp. Ex. F</b>	<b>Ex. 9</b>	<b>Comp. Ex. G</b>
PET with IPA	68.3	68.3	68.3	68.3
PTS	0.5	0.5	0.5	0.5
NAV 101	0.4		0.4	
Trisodium phosphate		0.4		0.4
EPON® 1009F	0.6	0.6	0.6	0.6
Irganox® 1010	0.2	0.2	0.2	0.2
PPG 3563	30	30	30	30
Transmittance (%) (after conditioning at 23 °C and 65% relative humidity for 24 h)	44	34		
Transmittance (%) (after conditioning at 80 °C and 95% relative humidity for 1000 h)			35	12
Initial weld strength (MPa)	15	13	12	1
Weld strength after conditioning (MPa)	13	6		

All ingredient quantities are given in weight percent based on the total composition.

## Discussion of the Examples

### 5    Example 1 and Comparative Example A

          Sodium montanate (NAV 101) (Example 1) and trisodium phosphate (Comparative Example A) were tested for moisture absorption as described above. Results are given in Table 1. These results clearly demonstrate that trisodium phosphate is not suitable for use in the present invention and that sodium montanate  
10    is suitable.

### Examples 2-7 and Comparative Examples B-E

          The compositions of Examples 2-7 and Comparative Examples B-E were prepared, molded, and tested as described above. The results are detailed in Tables  
15    2-4. Examples 2-7 demonstrate that when PET is melt-blended with the nucleating agents sodium montanate and sodium stearate, the resulting compositions can be easily molded and effectively laser welded. The crystallization half times given in Table 4 demonstrate that the compositions of Examples 2, 3, and 6 are effectively nucleated.

20           Comparative Examples B-E demonstrate that a poorly-dispersed polymeric nucleating agent, Surlyn® 8920, provides compositions that are not both easily molded and laser weldable. The low levels of Surlyn® used in Comparative Example B provide a composition with good laser weldability, but are not sufficient to adequately nucleate the PET, as is demonstrated by the long crystallization half time  
25    shown in Table 4. A comparison with Example 2 shows that the replacement of the Surlyn® of Comparative Example B with an equal amount of the sodium montanate of Example 2 gives a composition that is both effectively nucleated and has good laser weldability. A higher level of Surlyn® is used in Comparative Examples C-E, which gives materials that have good moldability. However, they also do not transmit  
30    a sufficiently high degree of light to permit effective laser welding.

### Examples 8 and 9 and Comparative Examples F and G

          The compositions of Examples 8 and 9 and Comparative Examples F and G were prepared by compounding the ingredients shown in Table 5 using the  
35    procedures given above. The compositions were molded into test pieces for laser welding as described above. Five test pieces were made for each experiment and the results given in Table 5 are averages of the results for each of the five pieces. In

the case of Example 8 and Comparative Example F, the initial light transmittance was determined on test pieces that had been conditioned for 24 hours at 23 °C and 65% relative humidity and is given in Table 5. These pieces were then, without further treatment, laser welded to pieces made from Rynite® 530 BK (which was first conditioned at 23 °C and 65% relative humidity for 24 hours) to make 10 bars each for the compositions of Example 8 and Comparative Example F. Five bars were conditioned for 24 hours at 23 °C and 65% relative humidity. The weld strengths were determined as described above and are given in Table 5 as "Initial weld strength." Five welded bars were conditioned at 80 °C and 95% relative humidity for 1000 hours and then at 23 °C and 65% relative humidity for 24 hours. The weld strengths of the bars were determined and are given as an average in Table 5 as "Weld strength after conditioning." The laser-welded bars incorporating the composition of Example 8, which uses sodium montanate, a nucleating agent of the present invention, maintained most of the weld strength of the bars that were not conditioned for 1000 hours and the resulting weld strength was still acceptable. The laser welded bars incorporating the composition of Comparative Example F, which uses trisodium phosphate, a nucleating agent outside the scope of the present invention, lost a substantial portion of the weld strength of the bars that were not conditioned for 1000 hours and the resulting weld strength was not acceptable.

In the case of Example 9 and Comparative Example G, the initial light transmittance was determined on test pieces that were conditioned at 80 °C and 95% relative humidity for 1000 hours and then at 23 °C and 65% relative humidity for 24 hours and is given in Table 5. These pieces were then laser welded to pieces made from Rynite® 530 BK (which was first conditioned at 23 °C and 65% relative humidity for 24 hours) as described above. After welding, the bars were conditioned at 23 °C and 65% relative humidity for 24 hours. The weld strengths were then determined as described above and are given in Table 5 as "Initial weld strength." The laser-welded bars incorporating the composition of Example 9, which uses sodium montanate, a nucleating agent of the present invention had an acceptable weld strength, despite the fact that the piece made from the composition of Example 9 had had long-term exposure to significant humidity prior to molding. The laser welded bars incorporating the composition of Comparative Example G, which uses trisodium phosphate, a nucleating agent outside the scope of the present invention had an unacceptable weld strength as a result of the long-term exposure to significant humidity experienced by the piece made from the composition of Comparative Example G.